
PREDICTING AIR TEMPERATURES IN CITY
STREETS ON THE BASIS OF MEASURED
REFERENCE DATA

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degree of Doctor of Philosophy

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APPENDICES

Appendix A: Calculation of view factors.

Appendix B: Calculation of shaded areas.

Appendix C: CAT code (FORTRAN)

APPENDIX A: CALCULATION OF VIEW FACTORS

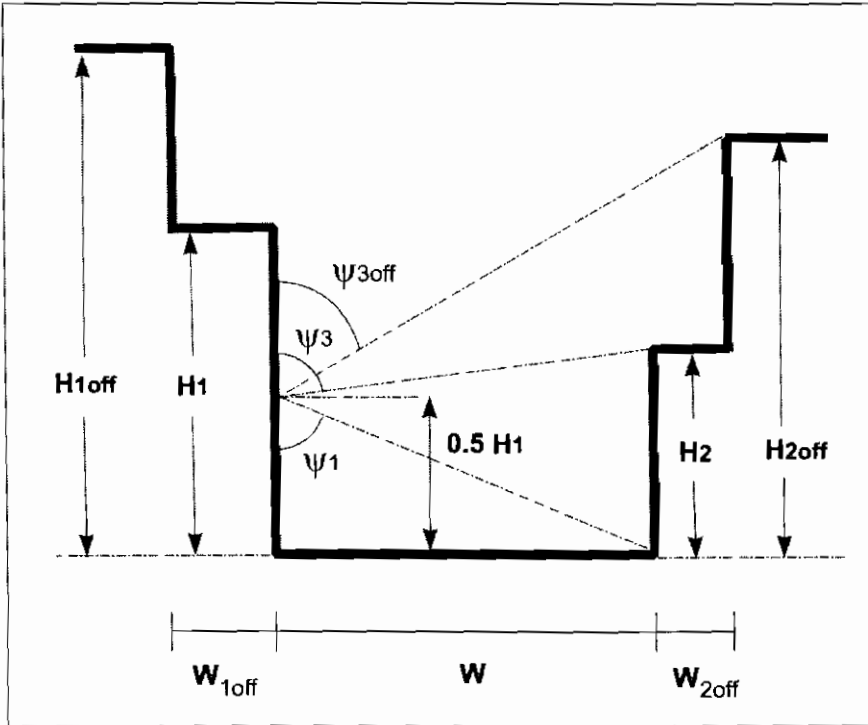


Figure 1: View factors from the middle of canyon wall 1

$$\Psi_1 = \text{ATAN}(W / (H_1 * 0.5))$$

$$\Psi_3 = \text{ATAN}(W / (H_2 - 0.5 * H_1)), \text{ but } \Psi_3 \text{ cannot exceed } \pi/2.$$

$$\Psi_{3off} = \text{ATAN}((W + W_{2off}) / (H_{2off} - (0.5 * H_1)))$$

$$VF_{w1_g} = 0.5 * (1 - \text{COS}(\Psi_1))$$

$$VF_{w1_w2} = 0.5 * (\text{COS}(\Psi_1) + \text{COS}(\Psi_3))$$

If $\Psi_{3off} < \Psi_3$, then

$$VF_{w1_s} = 0.5 * (1 - \text{COS}(\Psi_{3off}))$$

If $\Psi_{3off} > \Psi_3$, then

$$VF_{w1_s} = 0.5 * (1 - \text{COS}(\Psi_3))$$

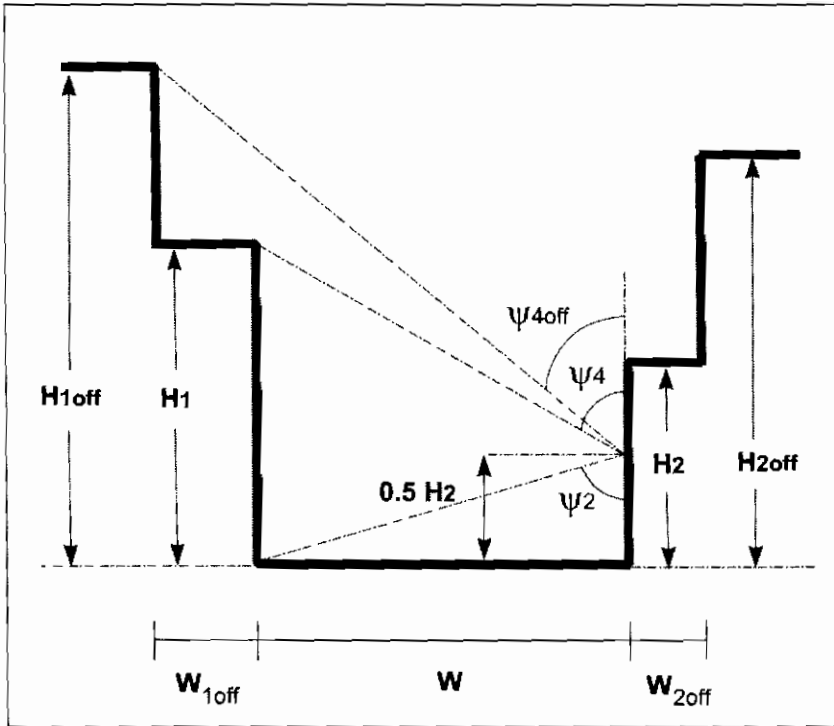


Figure 2: View factors from the middle of canyon wall 2

$$\Psi_2 = \text{ATAN}(W / (H_2 * 0.5))$$

$$\Psi_4 = \text{ATAN}(W / (H_1 - 0.5 * H_1)), \text{ but } \Psi_4 \text{ cannot exceed } \pi/2.$$

$$\Psi_{4off} = \text{ATAN}((W + W_{1off}) / (H_{1off} - (0.5 * H_2)))$$

$$VF_{w2_g} = 0.5 * (1 - \text{COS}(\Psi_2))$$

$$VF_{w2_w1} = 0.5 * (\text{COS}(\Psi_2) + \text{COS}(\Psi_4))$$

If $\Psi_{4off} < \Psi_4$, then

$$VF_{w2_s} = 0.5 * (1 - \text{COS}(\Psi_{4off}))$$

If $\Psi_{4off} > \Psi_4$, then

$$VF_{w2_s} = 0.5 * (1 - \text{COS}(\Psi_4))$$

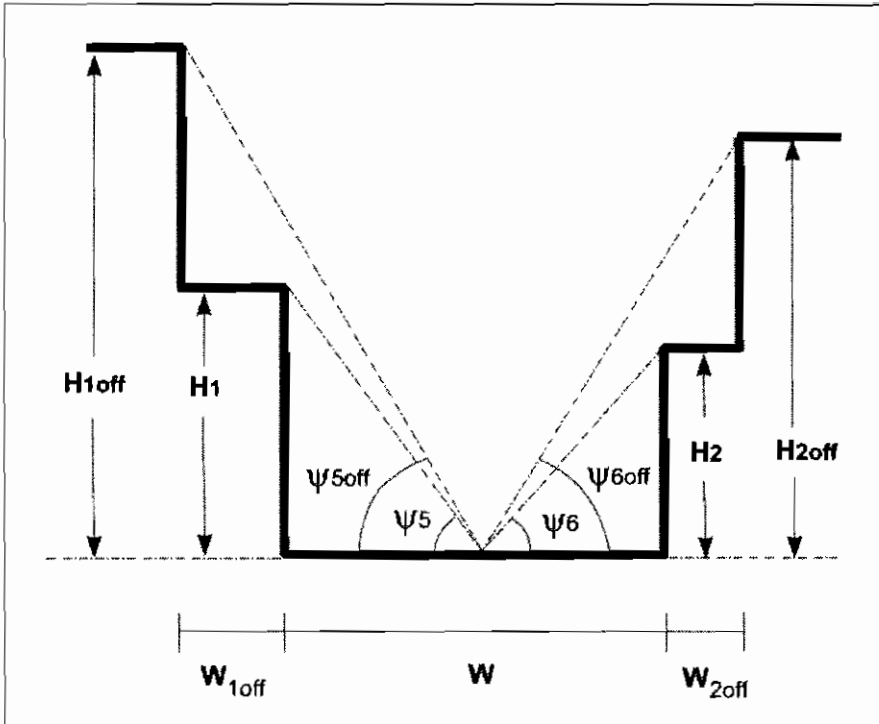


Figure 3: View factors from middle of canyon floor

$$\Psi_5 = \text{ATAN}(H_1 / (0.5 * W))$$

$$\Psi_6 = \text{ATAN}(H_2 / (0.5 * W))$$

$$\Psi_{5off} = \text{ATAN}(H_{1off} / (0.5 * W + W_{1off}))$$

$$\Psi_{6off} = \text{ATAN}(H_{2off} / (0.5 * W + W_{2off}))$$

$$VF_{g_w1} = 0.5 * (1 - \text{COS}(\Psi_5))$$

$$VF_{g_w2} = 0.5 * (1 - \text{COS}(\Psi_6))$$

To test for restriction of sky view factor by adjacent buildings taller than canyon walls, compare Ψ_5 with Ψ_{5off} and Ψ_6 with Ψ_{6off} .

If, as in Figure 3 above, $\Psi_{5off} > \Psi_5$ and $\Psi_{6off} > \Psi_6$, then

$$VF_{g_s} = 1 - [(1 - \text{COS}(\Psi_{5off})) + (1 - \text{COS}(\Psi_{6off}))]$$

APPENDIX B: CALCULATION OF SHADED AREAS

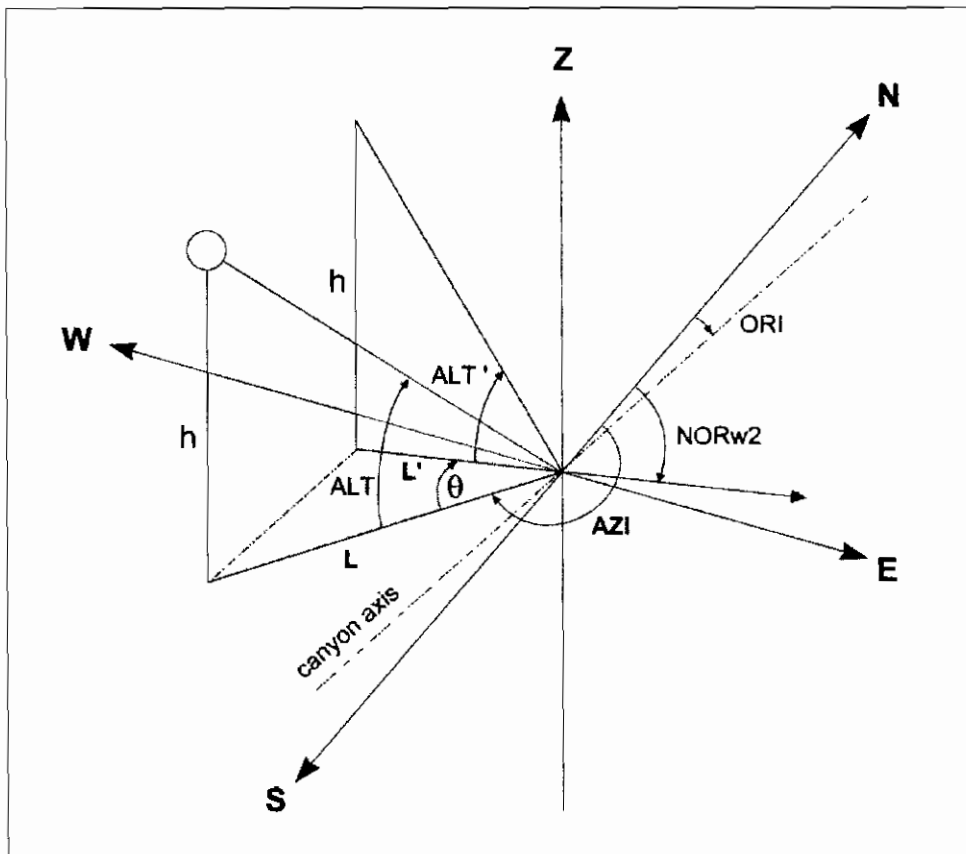


Figure 4: Projection of solar altitude (ALT) on plane perpendicular to canyon axis

$$\tan (ALT') = h/L'$$

$$\theta = |AZI - NORw2|$$

$$L' = L \cos \theta$$

$$h = L \tan (ALT)$$

$$\begin{aligned} \tan (ALT') &= L \tan (ALT) / L \cos \theta \\ &= \tan (ALT) / \cos \theta \end{aligned}$$

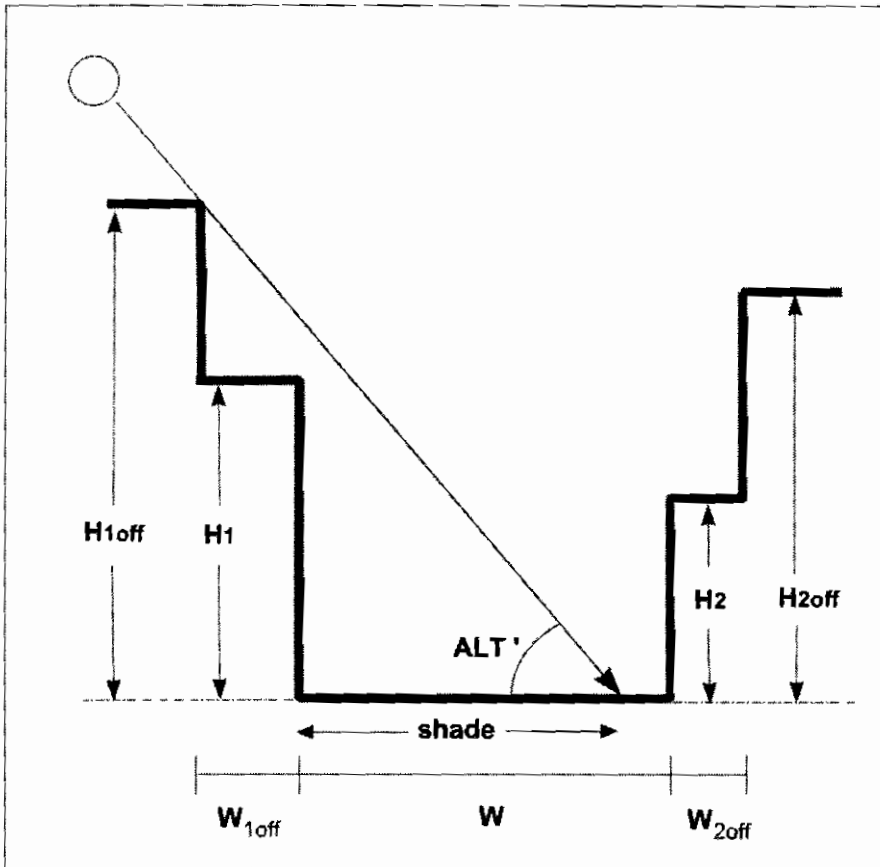


Figure 5: Shaded fraction of canyon floor resulting from obstruction of direct solar radiation by adjacent building

$$PSAg = \text{shade}/W$$

If the adjacent building casts the shadow,

$$\text{shade} = (H_{1off} / \tan (ALT')) - W_{1off}$$

$$PSAg = (([H_{1off} / \tan (ALT')] - W_{1off}) / W$$

but

$$\tan (ALT') = \tan (ALT) / \cos \theta$$

$$PSAg = ((H_{1off} * \cos \theta / \tan (ALT)) - W_{1off}) / W$$

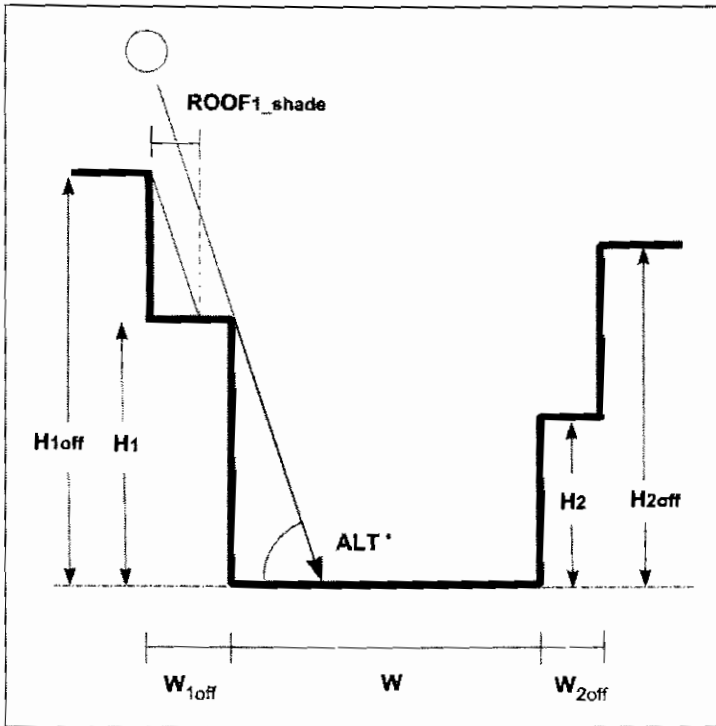


Figure 6: Shaded fraction of canyon floor resulting from obstruction of direct solar radiation by canyon wall

If the canyon wall casts the shadow,

$$\text{shade} = H_1 / \tan (ALT')$$

$$\text{PSAg} = H_1 / \tan (ALT') / W$$

but

$$\tan (ALT') = \tan (ALT) / \cos \theta$$

$$\text{PSAg} = (H_1 / W) * (\cos \theta / \tan (ALT))$$

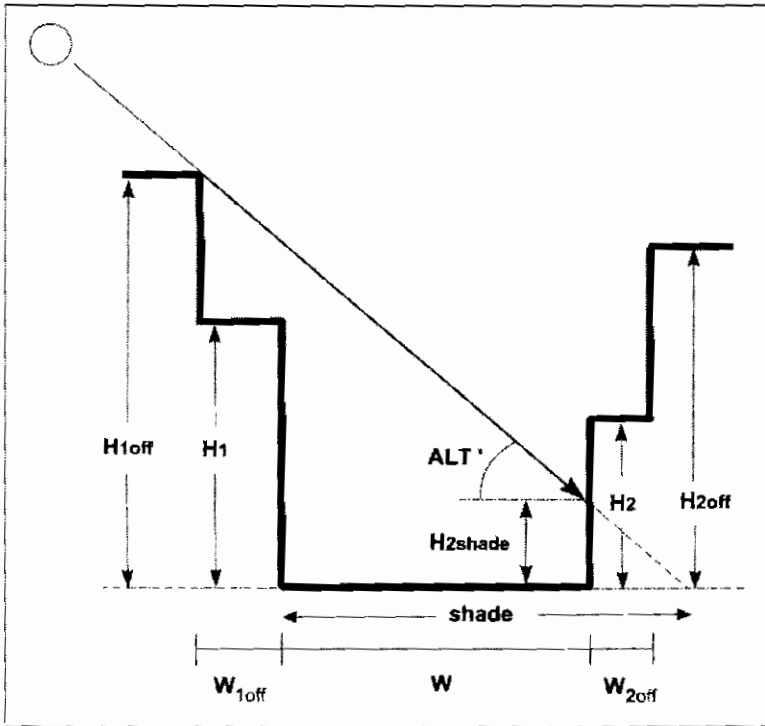


Figure 7: Shaded fraction of canyon wall resulting from obstruction of direct solar radiation by adjacent building

$$PSA_{w2} = H_{2shade}/H_2$$

If the adjacent tall building casts the shadow,

$$H_{2shade} = H_{1off} - \tan (ALT') * (W + W_{1off})$$

but

$$\tan (ALT') = \tan (ALT) / \cos \theta$$

$$PSA_{w2} = (1/H_2) * (H_{1off} - (\tan (ALT) / \cos \theta) * (W + W_{1off}))$$

If the other canyon wall casts the shadow,

$$PSA_{w2} = (1/H_2) * (H_1 - (\tan (ALT) / \cos \theta) * W)$$

APPENDIX C: CAT CODE (FORTRAN)

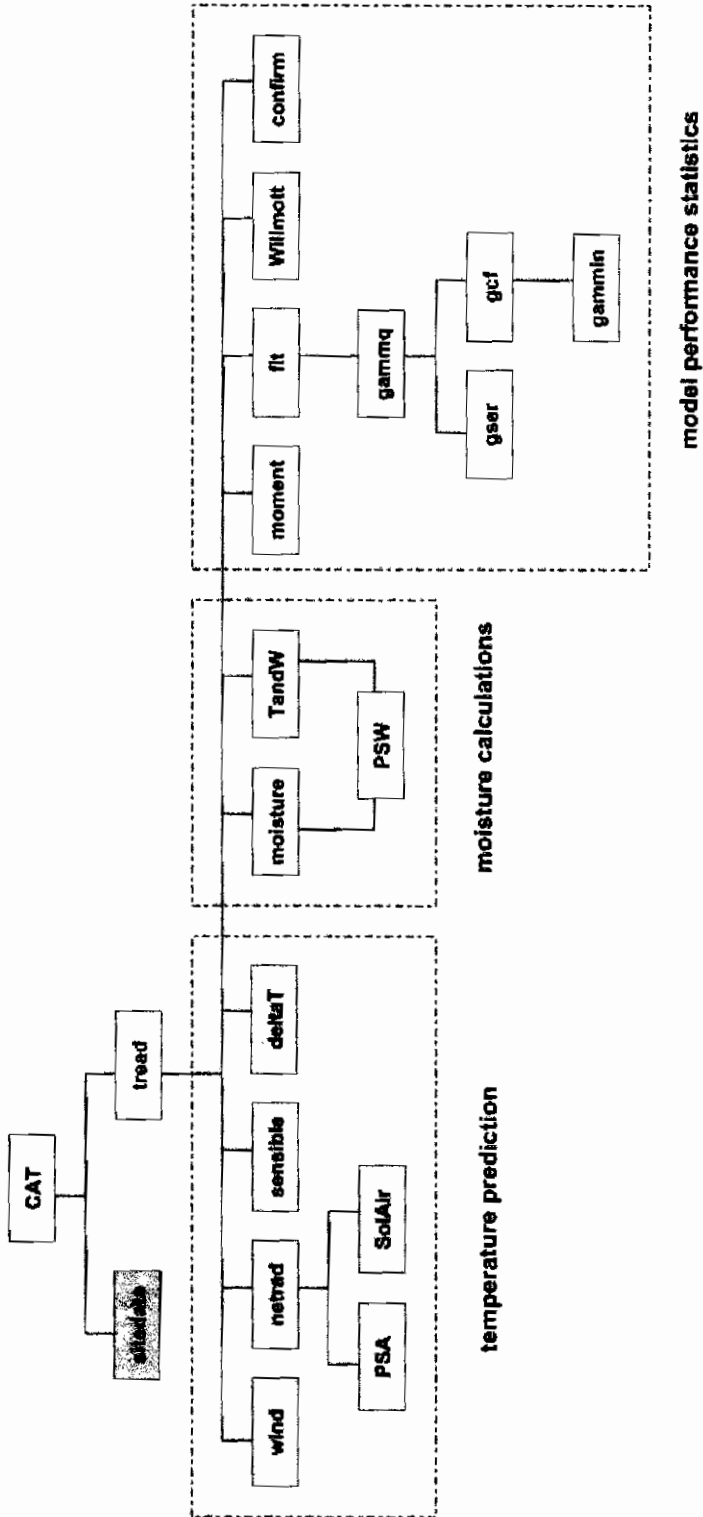


Figure C1: Structure of CAT program

PROGRAM CAT

c Version: 9_14

c Last change: EE September 6, 2004

```
REAL albed_met(2),A1_met(3),A2_met(3),A3_met(3)
REAL albed_urb(2),A1_urb(3),A2_urb(3),A3_urb(3)
REAL ORIdeg_met,W_met,H1_met,H2_met
REAL W1off_met,H1off_met,W2off_met,H2off_met
REAL ORIdeg_urb,W_urb,H1_urb,H2_urb
REAL W1off_urb,H1off_urb,W2off_urb,H2off_urb
REAL alpha_met,alpha_urb
REAL mix_met(4),mix_urb(4)
```

```
INTEGER IMS,IYS,IM,IY
```

- c Note: The overall structure of this program is based on previous
- c software by Williamson, especially with respect to data input and
- c initial processing. Theoretical basis for computation algorithms
- c of the micro-climate model is acknowledged in the relevant sections.
- c Statistic evaluation subroutines by Williamson.

```
print*,'*****'
print*,'
print*,'THIS PROGRAM CALCULATES CANYON AIR TEMPERATURE FROM
print*,'CLIMATIC DATA OF REFERENCE SITE
print*,'
print*,'IMS - START MONTH OF INPUT DATA
print*,'IYS - START YEAR OF INPUT DATA
print*,'IM - REQUIRED START MONTH FOR SELECTED DATA
print*,'IY - REQUIRED START YEAR FOR SELECTED DATA
print*,'
print*,'*****'
```

```
OPEN(UNIT=1,FILE='meteo_in.txt')
OPEN(UNIT=2,FILE='predict.txt')
OPEN(UNIT=4,FILE='met_site.txt')
OPEN(UNIT=7,FILE='urb_site.txt')
OPEN(UNIT=8,FILE='netrad.txt')
OPEN(UNIT=9,FILE='solair.txt')
OPEN(UNIT=11,FILE='ufluxes.txt')
c OPEN(UNIT=12,FILE='moisture.txt')
OPEN(UNIT=13,FILE='stats.txt')
OPEN(UNIT=14,FILE='averages.txt')
OPEN(UNIT=15,FILE='wind.txt')
OPEN(UNIT=16,FILE='mfluxes.txt')
```

```
PRINT 11
11 FORMAT(/,5x,' input IMS, IYS, IM, IY, NO OF MONTHS - ')
READ *, IMS,IYS,IM,IY,NMONTH
12 FORMAT(5I2)
```

- c read site parameters

```
print*
print*,'Reading site data for the weather data collection site.'

CALL SITEDATA(4,albed_met,W_met,H1_met,H2_met,
1 W1off_met,H1off_met,W2off_met,H2off_met,
```

```
2 ORIddeg_met,A1_met,A2_met,A3_met)
```

```
print*
```

```
print*,'Reading site data for the urban canyon site.'
```

```
CALL SITEDATA(7,albed_urb,W_urb,H1_urb,H2_urb,
```

```
1 W1off_urb,H1off_urb,W2off_urb,H2off_urb,
```

```
2 ORIddeg_urb,A1_urb,A2_urb,A3_urb)
```

- c Values for the mixing coefficient mix_met and mix_urb are still read
- c from files met_site.txt and urb_site.txt, but the values are not
- c used. Instead, identical values are used for both sites,
- c and are included in subroutine deltaT.

- c Read months prior to required period

```
IFLG=1
```

```
MNUM=IM-IMS+(IY-IYS)*12
```

```
IF(MNUM.EQ.0) GOTO 20
```

```
CALL TREAD(IMS,IYS,MNUM,IFLG,
```

```
1 albed_met,W_met,H1_met,H2_met,W1off_met,H1off_met,
```

```
2 W2off_met,H2off_met,ORIddeg_met,
```

```
3 albed_urb,W_urb,H1_urb,H2_urb,W1off_urb,H1off_urb,
```

```
4 W2off_urb,H2off_urb,ORIddeg_urb,
```

```
5 Ta_chesser,dTa_met,dTa_urb,Ta_base,Ta_urb,Qh_met,Qh_urb,
```

```
6 Alpha_met,Alpha_urb,mix_met,mix_urb,
```

```
7 A1_met,A2_met,A3_met,A1_urb,A2_urb,A3_urb)
```

- c Read data for required period

```
20 IFLG=2
```

```
CALL TREAD(IM,IY,NMONTH,IFLG,
```

```
1 albed_met,W_met,H1_met,H2_met,W1off_met,H1off_met,
```

```
2 W2off_met,H2off_met,ORIddeg_met,
```

```
3 albed_urb,W_urb,H1_urb,H2_urb,W1off_urb,H1off_urb,
```

```
4 W2off_urb,H2off_urb,ORIddeg_urb,
```

```
5 Ta_chesser,dTa_met,dTa_urb,Ta_base,Ta_urb,Qh_met,Qh_urb,
```

```
6 Alpha_met,Alpha_urb,mix_met,mix_urb,
```

```
7 A1_met,A2_met,A3_met,A1_urb,A2_urb,A3_urb)
```

```
CLOSE(UNIT=1)
```

```
CLOSE(UNIT=2)
```

```
CLOSE(UNIT=4)
```

```
CLOSE(UNIT=7)
```

```
CLOSE(UNIT=8)
```

```
CLOSE(UNIT=9)
```

```
CLOSE(UNIT=10)
```

```
CLOSE(UNIT=11)
```

- c CLOSE(UNIT=12)

```
CLOSE(UNIT=13)
```

```
CLOSE(UNIT=14)
```

```
CLOSE(UNIT=15)
```

```
CLOSE(UNIT=16)
```

STOP
END

C-----

```
SUBROUTINE TREAD (IMON,IYEAR,NMON,IFLG,  
1 albed_met,W_met,H1_met,H2_met,WIoff_met,H1off_met,  
2 W2off_met,H2off_met,ORIddeg_met,  
3 albed_urb,W_urb,H1_urb,H2_urb,WIoff_urb,H1off_urb,  
4 W2off_urb,H2off_urb,ORIddeg_urb,  
5 Ta_chesser,dTa_met,dTa_urb,Ta_base,Ta_urb,Qh_met,Qh_urb,  
6 Alpha_met,Alpha_urb,mix_met,mix_urb,  
7 A1_met,A2_met,A3_met,A1_urb,A2_urb,A3_urb)
```

- c This subroutine ties together the main program modules and
- c outputs predicted values for canyon air temperature.

```
REAL albed_met(2),mix_met(4),MIXING_met,SURFonW_met  
REAL albed_urb(2),mix_urb(4),MIXING_urb,SURFonW_urb  
REAL ORIddeg_met,ORIddeg_urb  
REAL Qstar_gurb,Qstar_w1urb,Qstar_w2urb  
REAL Qstar_gmet,Qstar_w1met,Qstar_w2met  
REAL Ta_met,Ta_urb,Ta_chesser,HeatD(12)  
REAL ALTdeg,AZIddeg,U10_met,RAIN  
REAL Qh_met,Qh_urb,Qe_met,Qe_urb,Ta_error,Qf  
REAL A1_met(3),A2_met(3),A3_met(3),A1_urb(3),A2_urb(3),A3_urb(3)  
REAL moist_met,moist_chesser,moist_base,moist_urb  
REAL Alpha_met,Alpha_urb  
REAL MAvail_met(12),MAvail_urb(12),Rt_met,Rt_urb
```

```
REAL Ta_met_min,Ta_chesser_min,Ta_urb_min  
REAL Ta_met_avg,Ta_chesser_avg,Ta_urb_avg  
REAL Ta_met_max,Ta_chesser_max,Ta_urb_max
```

```
REAL Ta_met_dmin(31),Ta_met_dmax(31)  
REAL Ta_urb_dmin(31),Ta_urb_dmax(31)  
REAL Ta_chesser_dmin(31),Ta_chesser_dmax(31)
```

```
INTEGER yy,mm,dd,hh  
INTEGER RH_met,RH_urb,Udeg_met,CLOUD,Iglob,Idif,RH_chesser  
INTEGER HOURCOUNT
```

```
LOGICAL RAIN_prev
```

```
REAL T_error(9000),T_predict(9000),T_obs(9000),T_input(9000),  
1 SIG(9000)
```

- c The data input for HeatD is anthropogenic heat, assuming constant
- c monthly value, in W m⁻² of canyon floor area.

```
c DATA HeatD/15,15,15,15,15,15,15,20,35,35,30,30,30,30,35,35,  
c 1 35,30,30,25,20,15,15/
```

```
DATA HeatD/15,15,15,20,30,35,35,35,30,25,15,15/
```

- c The data input for MAvail_met is moisture availability,

c assuming constant monthly values.

```
DATA MAvail_met/0.25,0.25,0.25,0.6,1.0,1.0,  
1 1.0,0.8,0.6,0.4,0.25,0.25/
```

c The data input for MAvail_urb is moisture availability,
c assuming constant monthly values.

```
DATA MAvail_urb/0.25,0.25,0.25,0.25,0.25,0.25,  
1 0.25,0.25,0.25,0.25,0.25,0.25/
```

c Initialise variables

```
RAIN_prev = .FALSE.  
HOURCOUNT=0  
mtempkount=0.  
Months_Done=0  
Qstar_gurb =0.  
Qstar_w1urb =0.  
Qstar_w2urb =0.  
Qstar_gmet =0.  
Qstar_w1met =0.  
Qstar_w2met =0.  
ERROR_max=0.  
ERROR_min=0.
```

```
T_error(9000) = 0.  
T_predict(9000) = 0.  
T_obs(9000) = 0.  
T_input(9000) =0.  
SIG(9000) =0.
```

```
Ta_met_min=100.  
Ta_chesser_min=100.  
Ta_urb_min=100.
```

```
Ta_met_max=0.  
Ta_chesser_max=0.  
Ta_urb_max=0.
```

```
Ta_met_avg=0.  
Ta_chesser_avg=0.  
Ta_urb_avg=0.
```

```
Ta_met_sum=0.  
Ta_chesser_sum=0.  
Ta_urb_sum=0.
```

```
do i=1,31  
  Ta_met_dmin(i)=100.  
  Ta_urb_dmin(i)=100.  
  Ta_chesser_dmin(i)=100.  
  Ta_met_dmax(i)=0.  
  Ta_urb_dmax(i)=0.  
  Ta_chesser_dmax(i)=0.  
end do
```

```
KStart=1
```

```
22 DO 7 K=Kstart,NMON
    Months_Done= Months_Done+1
```

```
    GOTO(10,20,10,30,10,30,10,10,30,10,30,10) IMON
10 IDAY=31
    GOTO 50
20 IDAY=28
    IF(IYEAR.EQ.88) IDAY=29
    IF(IYEAR.EQ.92) IDAY=29
    IF(IYEAR.EQ.96) IDAY=29
    IF(iyear.eq.00) Iday=29
    IF(iyear.eq.04) Iday=29
    GOTO 50
30 IDAY=30
50 NF=IDAY*24
```

```
60 DO 3 Icount=1,NF
```

c weather data from met station (and Chesset St. DBT and RH)

```
READ (1,*,END=90) YY,MM,DD,HH,Ta_met,RH_met,U10_met,Udeg_met,
1 Cloud,RAIN,Iglob,Idif,ALTdeg,AZIdeg,Ta_chesser,RH_chesser
```

```
IF(HH.eq.0) hh=24
```

```
IF(DD.eq.1.AND.HH.eq.1) then
    print*, 'Reading month ',MM
ENDIF
```

```
IF(HH.eq.1) then
    numday=(icount/24)+1
    print*, 'Reading day ',numday
ENDIF
```

```
IF(IFLG.EQ.1) GOTO 3
```

c If iflg=1 then only stepping through unwanted months
c so jump to end of subroutine.

```
c -----
c WIND CALCULATIONS FOR SURFACE COEFFICIENTS IN BOTH SITES
c -----
```

```
CALL WIND (W_urb,H1_urb,H2_urb,U10_met,Udeg_met,ORIdeg_urb,
1 Hc_gmet,Hc_wmet,Hc_gurb,Hc_wurb,Rt_met,Rt_urb)
```

```
c -----
c CALCULATIONS FOR REFERENCE SITE:
c -----
```

c Calculate net radiation for reference site:

```
CALL NETRAD (4,Ta_met,RH_met,CLOUD,Iglob,Idif,
1 H1_met,H2_met,W_met,H1off_met,H2off_met,
2 W1off_met,W2off_met,ORIdeg_met,AZIdeg,ALTdeg,Hc_gmet,HC_wmet,
```

```
3 Qstar_gmet,Qstar_w1met,Qstar_w2met,
4 Qstar_gmetprev,Qstar_w1metprev,Qstar_w2metprev,
5 albed_met(1),albed_met(2),Tsurf_met)
```

c Read appropriate monthly value for moisture availability (alpha)

alpha_met=MAvail_met(mm)

c Calculate sensible and latent heat flux in reference site:

```
CALL SENSIBLE (4,Ta_met,Qstar_gmet,Qstar_gmetprev,
1 dQstar_gmet,dQs_gmet,Qh_gmet,Qe_gmet,alpha_met,
2 A1_met(1),A2_met(1),A3_met(1),RAIN,RAIN_prev)
```

```
CALL SENSIBLE (4,Ta_met,Qstar_w1met,Qstar_w1metprev,
1 dQstar_w1met,dQs_w1met,Qh_w1met,Qe_w1met,alpha_met,
2 A1_met(2),A2_met(2),A3_met(2),RAIN,RAIN_prev)
```

```
CALL SENSIBLE (4,Ta_met,Qstar_w2met,Qstar_w2metprev,
1 dQstar_w2met,dQs_w2met,Qh_w2met,Qe_w2met,alpha_met,
2 A1_met(3),A2_met(3),A3_met(3),RAIN,RAIN_prev)
```

$Qh_met = (Qh_gmet * W_met + Qh_w1met * H1_met + Qh_w2met * H2_met) /$
 $1 (W_met)$

$Qe_met = (Qe_gmet * W_met + Qe_w1met * H1_met + Qe_w2met * H2_met) /$
 $1 (W_met)$

$SURFonW_met = (W_met + H1_met + H2_met) / W_met$
 $Vol_met = (W_met * (H1_met + H2_met) / 2.)$

c Calculate delta T for the reference site:

$dTsurf = (Tsurf_met - 273.15) - Ta_met$

```
CALL deltaT (Hc_gmet,Qh_met,dTa_met,mix_met,
1 SURFonW_met,Vol_met,MIXING_met,dTsurf,Qe_met,dMc_met)
```

c -----

c CALCULATIONS FOR URBAN CANYON:

c -----

c Calculate net radiation for urban canyon:

```
CALL NETRAD (7,Ta_met,RH_met,CLOUD,Iglob,Idif,
1 H1_urb,H2_urb,W_urb,H1off_urb,H2off_urb,
2 W1off_urb,W2off_urb,ORIddeg_urb,AZIddeg,ALTdeg,Hc_gurb,Hc_wurb,
3 Qstar_gurb,Qstar_w1urb,Qstar_w2urb,
4 Qstar_gurbprev,Qstar_w1urbprev,Qstar_w2urbprev,
5 albed_urb(1),albed_urb(2),Tsurf_urb)
```

c Read appropriate monthly value for moisture availability (alpha)

alpha_urb=MAvail_urb(mm)

- c Calculate sensible heat flux in urban canyon, beginning with individual surfaces:

```
CALL SENSIBLE (7,Ta_met,Qstar_gurb,Qstar_gurbprev,
1 dQstar_gurb,dQs_gurb,Qh_gurb,Qe_gurb,alpha_urb,
2 A1_urb(1),A2_urb(1),A3_urb(1),RAIN,RAIN_prev)
```

```
CALL SENSIBLE (7,Ta_met,Qstar_w1urb,Qstar_w1urbprev,
1 dQstar_w1urb,dQs_w1urb,Qh_w1urb,Qe_w1urb,alpha_urb,
2 A1_urb(2),A2_urb(2),A3_urb(2),RAIN,RAIN_prev)
```

```
CALL SENSIBLE (7,Ta_met,Qstar_w2urb,Qstar_w2urbprev,
1 dQstar_w2urb,dQs_w2urb,Qh_w2urb,Qe_w2urb,alpha_urb,
2 A1_urb(3),A2_urb(3),A3_urb(3),RAIN,RAIN_prev)
```

- c $Q_f = \text{HeatD}(\text{mm})$

- c The following correction for the diurnal pattern of anthropogenic heat is an approximation based on Sailor and Lu's (2004) paper in Atmospheric Environment.

```
IF(HH.GT.8 .AND. HH.LT.17) THEN
  Qf=HeatD(mm)
ELSE
  Qf=HeatD(mm)*0.5
ENDIF
```

- c Following is a test for rain in the previous hour, incorporated in increase value of moisture availability for current hour.

```
IF(RAIN.GT.0.5) THEN
  RAIN_prev = .TRUE.
ELSE
  RAIN_prev = .FALSE.
END IF
```

- c To add anthropogenic heat to the calculation, enable following expression for Q_h , which includes Q_f .

$$Q_{h_urb} = Q_f + \frac{(Q_{h_gurb} * W_{urb} + Q_{h_w1urb} * H1_{urb} + Q_{h_w2urb} * H2_{urb})}{1 + (W_{urb})}$$

$$Q_{e_urb} = \frac{(Q_{e_gurb} * W_{urb} + Q_{e_w1urb} * H1_{urb} + Q_{e_w2urb} * H2_{urb})}{1 + (W_{urb})}$$

- c Write fluxes to diagnostic files UFLUXES.TXT and MFLUXES.MET:

```
WRITE(11,559) mm,dd,hh,Qh_urb,Qstar_gurb,dQs_gurb,Qh_gurb,
1 Qstar_w1urb,dQs_w1urb,Qh_w1urb,Qstar_w2urb,dQs_w2urb,Qh_w2urb,
2 Qf
```

```
WRITE(16,559) mm,dd,hh,Qh_met,Qstar_gmet,dQs_gmet,Qh_gmet,
1 Qstar_w1met,dQs_w1met,Qh_w1met,Qstar_w2met,dQs_w2met,Qh_w2met
```

```
559 FORMAT(3(I5),11(F7.2))
```

c Calculate delta T for the urban canyon:

```
SURFonW_urb=(W_urb+H1_urb+H2_urb)/W_urb  
Vol_urb=(W_urb*(H1_urb+H2_urb)/2.)
```

```
CALL deltaT (Hc_gurb,Qh_urb,dTa_urb,mix_urb,  
1 SURFonW_urb,Vol_urb,MIXING_urb,dTsurf,Qe_urb,dMc_urb)
```

c Write wind data and calculated factors to diagnostic file WIND.TXT:

```
WRITE(15,589) mm,dd,hh,U10_met,Hc_gmet,Hc_wmet,  
1 Hc_gurb,Hc_wurb,mixing_met
```

```
589 FORMAT(3(I4),F5.1,4(f7.2),f5.2)
```

```
c -----  
c CALCULATIONS FOR CANYON AIR TEMPERATURE:  
c -----
```

c Calculate base temperature and then canyon air temperature.

c Concept from Elnahas and Williamson, 1997:

```
Ta_base=Ta_met-dTa_met  
Ta_urb=Ta_base+dTa_urb
```

c Assemble data for error statistics

```
Ta_error = Ta_chesser-Ta_urb
```

```
IF(Ta_error.GT.ERROR_max) ERROR_max=Ta_error  
IF(Ta_error.LT.ERROR_min) ERROR_min=Ta_error
```

```
HOURLCOUNT=HOURLCOUNT+1
```

```
T_error(HOURLCOUNT)=Ta_error  
T_predict(HOURLCOUNT) = Ta_urb  
T_Obs(HOURLCOUNT) = Ta_Chesser  
T_input(HOURLCOUNT) = Ta_met
```

```
IF (Ta_met.LT.Ta_met_min) Ta_met_min=Ta_met  
IF (Ta_met.GT.Ta_met_max) Ta_met_max=Ta_met
```

```
IF (Ta_chesser.LT.Ta_chesser_min) Ta_chesser_min=Ta_chesser  
IF (Ta_chesser.GT.Ta_chesser_max) Ta_chesser_max=Ta_chesser
```

```
IF (Ta_urb.LT.Ta_urb_min) Ta_urb_min=Ta_urb  
IF (Ta_urb.GT.Ta_urb_max) Ta_urb_max=Ta_urb
```

```
Ta_met_sum=Ta_met_sum+Ta_met  
Ta_met_avg=Ta_met_sum/HOURLCOUNT
```

```
Ta_chesser_sum=Ta_chesser_sum+Ta_chesser  
Ta_chesser_avg=Ta_chesser_sum/HOURLCOUNT
```

```
Ta_urb_sum=Ta_urb_sum+Ta_urb
Ta_urb_avg=Ta_urb_sum/HOURCOUNT
```

```
IF (Ta_met.LT.Ta_met_dmin(dd)) Ta_met_dmin(dd)=Ta_met
IF (Ta_urb.LT.Ta_urb_dmin(dd)) Ta_urb_dmin(dd)=Ta_urb
IF (Ta_chesser.LT.Ta_chesser_dmin(dd)) THEN
  Ta_chesser_dmin(dd)=Ta_met
END IF
IF (Ta_met.GT.Ta_met_dmax(dd)) Ta_met_dmax(dd)=Ta_met
IF (Ta_urb.GT.Ta_urb_dmax(dd)) Ta_urb_dmax(dd)=Ta_urb
IF (Ta_chesser.GT.Ta_chesser_dmax(dd)) THEN
  Ta_chesser_dmax(dd)=Ta_chesser
END IF
```

```
c -----
c  CALCULATIONS FOR MOISTURE CONTENT:
c -----
```

- c First calculate moisture content from DBT and RH.
- c Data for Chesser site used for program validation only.

```
CALL MOISTURE (1013.25,Ta_met,RH_met,moist_met)
```

```
CALL MOISTURE (1013.25,Ta_chesser,RH_chesser,moist_chesser)
```

```
moist_base=moist_met-dMc_met
moist_urb=moist_base+dMc_urb
```

```
CALL TandW (Ta_urb,moist_urb,RH_urb)
```

```
c PRINT*,"Ta_met,RH_met,Ta_urb,RH_urb"
c print*,Ta_met,RH_met,Ta_urb,RH_urb
c PRINT*,"dMc_met,dMc_urb,moist_met,moist_chesser,moist_urb"
c print*,dMc_met,dMc_urb,moist_met,moist_chesser,moist_urb
c pause
```

- c Write moisture to diagnostic file MOISTURE.TXT

```
WRITE(12,560) mm,dd,hh,Ta_met,RH_met,moist_met,
1 Ta_chesser,RH_chesser,moist_chesser,Ta_urb,RH_urb,moist_urb
```

```
560 FORMAT(1x,3I5,3(f7.2,I5,f8.4))
```

- c Write data to output file PREDICT.TXT:

```
WRITE(2,120) yy,mm,dd,hh,Ta_met,U10_met,Udeg_met,Cloud,
1 Iglob,Idif,Ta_chesser,Ta_base,Ta_urb,Ta_error,
2 dTa_met,dTa_urb
```

```
120 FORMAT(4(I3),2(F5.1),I4,I2,2(I5),3(F5.1),F6.1,2(F5.1))
```

```
mtempkount=mtempkount+1
```

3 CONTINUE

```
imon=imon+1
IF(imon.GT.12) THEN
  imon=1
  iyear=iyear+1
ENDIF
```

7 CONTINUE

```
IF(IFLG.EQ.1) GOTO 99
```

c check if all months are done, rewind or exit

```
90 IF (Months_Done.ne.NMON) THEN
  REWIND 1
  imon=imon+1
  IF(imon.GT.12) THEN
    imon=1
  ENDIF
```

```
Kstart=Months_Done+1
GOTO 22
ELSE
CONTINUE
ENDIF
```

```
DO dd=1,31
  Ta_met_dmin_sum=Ta_met_dmin_sum+Ta_met_dmin(dd)
  Ta_urb_dmin_sum=Ta_urb_dmin_sum+Ta_urb_dmin(dd)
  Ta_chesser_dmin_sum=Ta_chesser_dmin_sum+Ta_chesser_dmin(dd)
  Ta_met_dmax_sum=Ta_met_dmax_sum+Ta_met_dmax(dd)
  Ta_urb_dmax_sum=Ta_urb_dmax_sum+Ta_urb_dmax(dd)
  Ta_chesser_dmax_sum=Ta_chesser_dmax_sum+Ta_chesser_dmax(dd)
END DO
```

```
Ta_met_dmin_avg=Ta_met_dmin_sum/lday
Ta_urb_dmin_avg=Ta_urb_dmin_sum/lday
Ta_chesser_dmin_avg=Ta_chesser_dmin_sum/lday
Ta_met_dmax_avg=Ta_met_dmax_sum/lday
Ta_urb_dmax_avg=Ta_urb_dmax_sum/lday
Ta_chesser_dmax_avg=Ta_chesser_dmax_sum/lday
```

```
CALL MOMENT(T_error,HOURCOUNT,AVE,ADEV,SDEV,VAR,SKEW,CURT)
```

c
c Calculate Willmott statistics

c
c initial SIG to zero values
c set mwt =0

c
do i=1,9000
sig(i)=0.
end do

c
mwt=0.

```
CALL FIT(T_obs,T_predict,HOURCOUNT,SIG,mwt,A,B,SIGA,SIGB,CHI2,Q)
```

```

c calculate Willmott systematic and unsystematic errors (RMSEs & RMSEu)
c and index of agreement (d)
c
  call Willmott(T_predict,T_obs,HOURCOUNT,A,B,RMSE,RMSEs,RMSEu,d,
  1 wMSE,wMSEs,wMSEu)

  call Confirm(T_predict,T_obs,T_input,HOURCOUNT,Theil,DofC)
c PRINT*,"U= ",U,"D= ",DofC

```

```

PRINT*,
PRINT*,'*****'
PRINT*,' ERROR STATISTICS'
PRINT*,'*****'
PRINT*,
PRINT 100, HOURCOUNT
100 FORMAT ( 5x,'total number of hours   = ',I5)
  PRINT 101,AVE
101 FORMAT ( 5x,'mean error               = ',F5.2)
  PRINT 102,SDEV
102 FORMAT ( 5x,'standard deviation       = ',F5.2)
  PRINT 103,ERROR_max
103 FORMAT ( 5x,'maximum error            = ',F5.2)
  PRINT 104,ERROR_min
104 FORMAT ( 5x,'minimum error            = ',F5.2)
  PRINT 105,wMSE
105 FORMAT ( 5x,'MSE                      = ',F6.3)
  PRINT 106,wMSEs
106 FORMAT ( 5x,'systematic MSE           = ',F6.3)
  PRINT 107,wMSEu
107 FORMAT ( 5x,'unsystematic MSE        = ',F6.3)
  PRINT 108,d
108 FORMAT ( 5x,'Willmott index           = ',F6.3)
  PRINT 109,Theil
109 FORMAT ( 5x,'Theil inequality coeff.  = ',F6.3)
  PRINT 110,DofC
110 FORMAT ( 5x,'degree of confirmation   = ',F6.3)
PRINT*,

```

```

PRINT*,'Data below only valid for simulation of single months.'
PRINT*,
PRINT*,'          City   City'
PRINT*,'          BoM   obs.   pred.'
PRINT 111,Ta_met_min,Ta_chesser_min,Ta_urb_min
111 FORMAT (5x,'abs. monthly min',4x,F5.2,6x,F5.2,6x,F5.2)
  PRINT 112,Ta_met_dmin_avg,Ta_chesser_dmin_avg,
  1 Ta_urb_dmin_avg
112 FORMAT (5x,'mean monthly min',4x,F5.2,6x,F5.2,6x,F5.2)
  PRINT 113,Ta_met_avg,Ta_chesser_avg,Ta_urb_avg
113 FORMAT (5x,'monthly avg',9x,F5.2,6x,F5.2,6x,F5.2)
  PRINT 114,Ta_met_dmax_avg,Ta_chesser_dmax_avg,
  1 Ta_urb_dmax_avg
114 FORMAT (5x,'mean monthly max',4x,F5.2,6x,F5.2,6x,F5.2)
  PRINT 115,Ta_met_max,Ta_chesser_max,Ta_urb_max
115 FORMAT (5x,'abs. monthly max',4x,F5.2,6x,F5.2,6x,F5.2)
PRINT*,
PRINT*,'*****'

```

```

WRITE (13,100) HOURCOUNT

```

```

WRITE (13,101) AVE
WRITE (13,102) SDEV
WRITE (13,103) ERROR_max
WRITE (13,104) ERROR_min
WRITE (13,105) wMSE
WRITE (13,106) wMSEs
WRITE (13,107) wMSEu
WRITE (13,108) d
WRITE (13,109) Theil
WRITE (13,110) DofC
WRITE (14,111) Ta_met_min,Ta_chesser_min,Ta_urb_min
WRITE (14,112) Ta_met_dmin_avg,Ta_chesser_dmin_avg,
1 Ta_urb_dmin_avg
WRITE (14,113) Ta_met_avg,Ta_chesser_avg,Ta_urb_avg
WRITE (14,114) Ta_met_dmax_avg,Ta_chesser_dmax_avg,
1 Ta_urb_dmax_avg
WRITE (14,115) Ta_met_max,Ta_chesser_max,Ta_urb_max

```

```

99 RETURN
END

```

c-----

```

SUBROUTINE NETRAD (SITE,Ta,RH,CLOUD,Iglob,Idif,
1 H1,H2,W,H1off,H2off,
2 W1off,W2off,ORIdeg,AZIdeg,ALTdeg,Hc_g,Hc_w,
3 Qstarg,Qstarw1,Qstarw2,Qstarg_prev,Qstarw1_prev,Qstarw2_prev,
4 ALBEDOg,ALBEDOw1,Tsol_g)

```

c This subroutine calculates net radiation on surfaces of canyon from
c measured air DBT, RH, wind speed and wind direction, cloud cover,
c and global and diffuse solar radiation.

```

REAL Ta,TaK,Pw,Pws,ORI,AZI,ALT,
1 Ibeam,CL10,
2 Hc_g, Hc_w,Hcr_g,Hcr_w,
3 Esky,Esurf,Lclear,Lsky,
4 NORw1,NORw2,ALBEDOg,ALBEDOw1,ALBEDOw2,
5 VFg_s,VFg_w1,VFg_w2,VFw1_s,VFw1_g,VFw1_w2,VFw2_s,VFw2_g,VFw2_w1,
6 Kg,Kdirg,Krefg,Kdifg,Kw1,Kdirw1,Kdifw1,
7 Krefw1,Kw2,Kdirw2,Kdifw2,Krefw2,
8 Qstarg,Qstarw1,Qstarw2,
9 H1,H2,W,H1off,H2off,W1off,W2off,AZIdeg,ALTdeg,ORIdeg,Tsol_g

```

```

DOUBLE PRECISION C8,C9,C10,C11,C12,C13,logPws,TaK_D

```

```

INTEGER SITE,CLOUD,RH,Iglob,Idif

```

c TIME VARIABLE (ENVIRONMENTAL) INPUTS:
c Ta is air DBT (deg C)
c RH is relative humidity (%)
c U10_met is wind speed at ten metre height (m s-1)
c Udeg is wind direction (degrees)
c CLOUD is cloud cover (tenths)
c Iglob is global radiation on a horizontal surface (W m-2)
c Ibeam is beam (normal) radiation (W m-2)
c Idif is diffuse radiation on a horizontal surface (W m-2)
c AZIdeg is solar azimuth (degrees)

c ALTdeg is solar elevation (degrees)

c CONSTANT INPUTS:

c W is canyon width (m)

c H1 is height of canyon wall 1 (m)

c H2 is height of canyon wall 2 (m)

c H1off is height of building adjacent to wall 1 (m)

c H2off is height of building adjacent to wall 2 (m)

c W1off is offset of building adjacent to wall 1 (m)

c W2off is offset of building adjacent to wall 2 (m)

c ALBEDOg is albedo of ground

c ALBEDOw1 is albedo of wall 1

c ALBEDOw2 is albedo of wall 2

c Esurf is long wave emissivity of surface

c ORIdeg is canyon orientation (degrees)

c Zd is zero plane displacement (m)

c Z0 is roughness length (m)

c Zr is height of anemometer (m)

c CONSTANTS CALCULATED BY PROGRAM:

c ORI is canyon orientation (radians)

c NORw1 is normal to wall 1 (radians)

c NORw2 is normal to wall 2 (radians)

c VFg_s is view factor from ground to sky

c VFg_w1 is view factor from ground to wall 1

c VFg_w2 is view factor from ground to wall 2

c VFw1_s is view factor from wall 1 to sky

c VFw1_g is view factor from wall 1 to ground

c VFw1_w2 is view factor from wall 1 to wall 2

c VFw2_s is view factor from wall 2 to sky

c VFw2_g is view factor from wall 2 to ground

c VFw2_w1 is view factor from wall 2 to wall 1

c VARIABLES CALCULATED BY PROGRAM:

c AZI is solar azimuth (radians)

c ALT is solar elevation (radians)

c TaK is air DBT (K)

c Tsol is sol-air temperature (K)

c Tsurf is surface temperature calculated from sol-air (K)

c Pw is partial pressure of water vapour (Pa)

c Pws is partial pressure of water vapour at saturation (Pa)

c Ustar is friction velocity (m s⁻¹)

c Hc is surface convective heat exchange coef. (W m⁻² K⁻¹)

c Esky is sky emissivity

c Lclear is clear sky long wave radiation (W m⁻²)

c Lsky is cloudy sky long wave radiation (W m⁻²)

c Lstar is net long wave radiation at the surface (W m⁻²)

c Lsurf is long wave radiation emitted by surface (W m⁻²)

c Kdown is solar radiation on surface (W m⁻²)

c Kstar is net shortwave radiation at the surface (W m⁻²)

c Kdirg is direct solar radiation on canyon floor (W m⁻²)

c Krefg is reflected solar radiation on canyon floor (W m⁻²)

c Kdifg is diffuse solar radiation on canyon floor (W m⁻²)

c Kg is total solar radiation on canyon floor (W m⁻²)

c Kdirw1 is direct solar radiation on wall1 (W m⁻²)

c Krefw1 is reflected solar radiation on wall 1 (W m⁻²)

c Kdifw1 is diffuse solar radiation on wall 1 (W m⁻²)

c Kw1 is total solar radiation on wall 1 (W m⁻²)

c Kdirw2 is direct solar radiation on wall 2 (W m⁻²)

- c Krefw2 is reflected solar radiation on wall 2 (W m-2)
- c Kdifw2 is diffuse solar radiation on wall 2 (W m-2)
- c Kw2 is total solar radiation on wall 2 (W m-2)
- c PSAg is partial shaded area ground
- c PSAw1 is partial shaded area of wall 1
- c PSAw2 is partial shaded area of wall 2
- c Qstarg, Qstarw1 and Qstarw2 are net radiation at ground and walls (W m-2)

c Universal constants:

PI=3.1415926
SIGMA = 5.67E-08

c At this stage, assign equal albedo for both walls:

ALBEDOw2=ALBEDOw1

```
IF (ORIdeg.LE.90) THEN
  ORI=ORIdeg*0.017453
ELSE
  ORI=(360-ORIdeg)*(-0.017453)
ENDIF
```

c Normal to walls required for solar radiation on wall surfaces:

```
IF (ORILT.0) THEN
  NORw1=ORI+(PI/2)
  NORw2=ORI-(PI/2)
ELSE
  NORw1=ORI-(PI/2)
  NORw2=ORI+(PI/2)
ENDIF
```

c Calculate view factors using six angles:

- c PSI1 is view angle from middle of wall 1 to canyon floor
- c PSI2 is view angle from middle of wall 2 to canyon floor
- c PSI3 is view angle from middle of wall 1 to sky
- c PSI4 is view angle from middle of wall 2 to sky
- c PSI5 is view angle from middle of canyon floor to wall 1
- c PSI6 is view angle from middle of canyon floor to wall 2

```
PSI1=ATAN(W/(H1*0.5))
PSI2=ATAN(W/(H2*0.5))
PSI3=ATAN(W/(H2-0.5*H1))
PSI4=ATAN(W/(H1-0.5*H2))
PSI5=ATAN(H1/(0.5*W))
PSI6=ATAN(H2/(0.5*W))
```

c Calculate view factors:

```
VFg_w1=0.5*(1-COS(PSI5))
VFg_w2=0.5*(1-COS(PSI6))

VFw1_g=0.5*(1-COS(PSI1))
VFw1_w2=0.5*(COS(PSI1)+COS(PSI3))
```



```
VFw2_g=0.5*(1-COS(PSI2))
VFw2_w1=0.5*(COS(PSI2)+COS(PSI4))
```

```
c *****Diagnostic*****
c Print*,'v.factors',VFg_w1,VFg_w2,VFw1_g,VFw1_w2,VFw2_g,VFw2_w1
c PAUSE
c *****
```

c Now test for restriction of view factor to sky by adjacent buildings:

```
PSI3off=ATAN((W+W2off)/(H2off-(0.5*H1)))
IF (PSI3off.LT.PSI3) PSI3=PSI3off
```

```
PSI4off=ATAN((W+W1off)/(H1off-(0.5*H2)))
IF (PSI4off.LT.PSI4) PSI4=PSI4off
```

```
PSI5off=ATAN(H1off/(0.5*W+W1off))
IF (PSI5off.GT.PSI5) PSI5=PSI5off
```

```
PSI6off=ATAN(H2off/(0.5*W+W2off))
IF (PSI6off.GT.PSI6) PSI6=PSI6off
```

```
VFg_s=1-(1-(COS(PSI5)+COS(PSI6))/2)
VFw1_s=0.5*(1-COS(PSI3))
VFw2_s=0.5*(1-COS(PSI4))
```

```
c -----
c First calculate long wave radiation from sky:
c -----
```

c constants C8 through C13 are used to calculate vapour pressure (Pw).

```
C8 = -5.8002206E+03
C9 = 1.391449
C10 = -4.864023E-02
C11 = 4.176476E-05
C12 = -1.445209E-08
C13 = 6.545967
```

c calculate partial pressure of water vapour, Pw (Pa),
c from ASHRAE Fundamentals Chapter 6

```
TaK=Ta+273.15
TaK_D= DBLE(TaK)
logPws =C8/TaK_D+C9+C10*TaK_D+C11*TaK_D**2+C12*TaK_D**3+
1 C13*DLOG(TaK_D)
Pws = SNGL(EXP(logPws))
Pw = Pws*RH/100
```

c To convert Pw in Pa to hPa (mb), divide by 100
Pw_mb = Pw/100.

c Atmospheric emissivity calculated from Brutsaert, 1982:

```
Esy = 1.24*(Pw_mb/TaK)**(1./7.)
```

```
Lclear = SIGMA*Esy*TaK**4
```

c Cloud correction from Martin, in Cook (ed) Passive Cooling, 1989:

c Note CLOUD cover in tenths

CL10 = FLOAT(CLOUD)

Lsky = Lclear*(1+0.0224*CL10-0.0035*CL10**2+0.00028*CL10**3)

c CALL WIND (SITE,W,H1,H2,U10,Udeg,Hcr_g,Hcr_w,Hc,ORIddeg,TaK)

c -----

c Calculate incoming solar radiation on each canyon surface:

c -----

c First convert apparent solar position from degrees to radians.

c (Solar azimuth is represented as radians east or west of north.)

IF (AZIddeg.LT.180) THEN

 AZI=AZIddeg*0.017453

ELSE

 AZI=-(2.*PI-AZIddeg*0.017453)

ENDIF

ALT=ALTdeg*0.017453

IF (ALT.lt.1E-04) THEN

 ALT=0.01

ENDIF

Ibeam=(FLOAT(Iglob)-FLOAT(Idif))/SIN(ALT)

IF(Ibeam.LT.0) THEN

 Ibeam=0

ENDIF

c Calculate proportion of each surface shaded

c from direct solar radiation:

CALL PSA (H1,H2,W,H1off,H2off,

1 W1off,W2off,ALT,AZI,PI,

2 Iglob,NORw1,PSAg,PSAw1,PSAw2)

c direct radiation on canyon surfaces

Kdirg=Ibeam*(1-PSAg)*SIN(ALT)

IF (ABS(AZI-NORw1).LT.(PI/2)) THEN

 Kdirw1=Ibeam*(1-PSAw1)*COS(ALT)*SIN(ABS(AZI-NORw1))

ELSE

 Kdirw1=0

ENDIF

IF (ABS(AZI-NORw2).LT.(PI/2)) THEN

 Kdirw2=Ibeam*(1-PSAw2)*COS(ALT)*SIN(ABS(AZI-NORw2))

ELSE

 Kdirw2=0

END IF

c diffuse radiation on canyon surfaces

```
Kdifg=float(Idif)*VFg_s
Kdifw1=float(Idif)*VFw1_s
Kdifw2=float(Idif)*VFw2_s
```

c reflected radiation on canyon surfaces

```
Krefg=(Kdirw1+Kdifw1)*ALBEDOw1*VFg_w1
1+(Kdirw2+Kdifw2)*ALBEDOw2*VFg_w2
```

```
Krefw1=(Kdirg+Kdifg)*ALBEDOg*VFw1_g
1+(Kdirw2+Kdifw2)*ALBEDOw2*VFw1_w2
```

```
Krefw2=(Kdirg+Kdifg)*ALBEDOg*VFw2_g
1+(Kdirw1+Kdifw1)*ALBEDOw1*VFw2_w1
```

c total incoming solar radiation on canyon surfaces

```
Kg=(Kdirg+Kdifg+Krefg)
Kw1=(Kdirw1+Kdifw1+Krefw1)
Kw2=(Kdirw2+Kdifw2+Krefw2)
```

```
c *****Diagnostic*****
c Print*, lbeam, Idif, Kg, Kw1, Kw2
c pause
c *****
```

c Now begin loop for numeric solution of approx. surface temperature
c using sol-air temperature formula.
c Use uniform long wave emissivity for all surfaces:

```
Esurf=0.95
```

```
Qstarg_prev=Qstarg
Qstarw1_prev=Qstarw1
Qstarw2_prev=Qstarw2
```

c Add radiative component to convective coeff. for total surface coeff.

```
Hr = 4.*0.9*sigma*TaK**3.
```

```
Hcr_g=Hc_g+Hr
Hcr_w=Hc_w+Hr
```

```
CALL SOLAIR(SITE,Lsky,Kg,TaK,Qstarg,Hcr_g,Esurf,ALBEDOg,VFg_s,
1 Tsol_g)
```

```
CALL SOLAIR(SITE,Lsky,Kw1,TaK,Qstarw1,Hcr_w,Esurf,ALBEDOw1,VFw1_s,
1 Tsol_w1)
```

```
CALL SOLAIR(SITE,Lsky,Kw2,TaK,Qstarw2,Hcr_w,Esurf,ALBEDOw2,VFw2_s,
1 Tsol_w2)
```

```

c *****Diagnostic*****
c   Print*, Qstarg,Qstarw1,Qstarw2
c   pause
c *****

```

```

c Write solar radiation on canyon surfaces to diagnostic file
c NETRAD.TXT:

```

```

WRITE(8,800) SITE,Iglob,Idif,Kdirg,Krefg,Kdifg,Kg,
1 Kdirw1,Krefw1,Kdifw1,Kw1,Kdirw2,Krefw2,Kdifw2,Kw2,
2 Qstarg,Qstarw1,Qstarw2,Tsol_g,Tsol_w1,Tsol_w2

```

```
800 FORMAT(I3,2(I4),18(F7.1))
```

```

RETURN
END

```

```
*****
```

```

SUBROUTINE SOLAIR (SITE,Lsky_d,K,TaK_d,Qstar,
1 Hconrad,Esurf_d,ALBEDO,VF,Tsurf)

```

```

REAL Lsky_d,Lsurf,Lstar,Kstar,K,TaK_d,Tsurf,Tsol,
1 Qstar,Hconrad,ALBEDO,SIGMA,VF

```

```
INTEGER SITE
```

```

c This subroutine calculates the sol-air temperature of a surface.
c The sol-air temperature is used as a surrogate for the actual
c temperature of the surface.

```

```
SIGMA=5.67E-08
```

```
Lsurf=SIGMA*Esurf_d*Tak_d**4
```

```

c The following statement assumes no NET exchange
c with other canyon surfaces:

```

```

Lstar=(Lsky_d-Lsurf)*VF
Kstar=K*(1-ALBEDO)

```

```

Tsurf=TaK_d
Tsol=TaK_d+(Kstar+Lstar)/Hconrad

```

```
KOUNT=0
```

```
99 ERROR=ABS(Tsol-Tsurf)
```

```
IF (KOUNT.eq.50) goto 98
```

```
IF (ERROR.GT.1.0) THEN
```

```

KOUNT=KOUNT+1
Tsurf=Tsurf+0.5*(Tsol-Tsurf)
Lsurf=Sigma*Esurf_d*Tsurf**4
Lstar=(Lsky_d-Lsurf)*VF
Tsol=TaK_d+(Kstar+Lstar)/Hconrad
GO TO 99
END IF
GO TO 97

```

```

98 PRINT*, 'solair did not converge'
STOP

```

```

97 Qstar=Kstar+Lstar

```

c Write interim radiation values used in calculation of sol-air
c temperature to diagnostic file SOLAIR.TXT:

```

write (9,401) SITE,K,Kstar,Lstar,Lsurf,Tsol
401 FORMAT(I2,5(F10.3))
RETURN

```

```

END

```

```

SUBROUTINE WIND (W_urb,H1_urb,H2_urb,WIND10,WINDdeg,ORIddeg,
1 Hc_gmet,Hc_wmet,Hc_gurb,Hc_wurb,Rtop_met,Rtop_urb)

```

c This subroutine calculates wind speed near the surfaces of an urban
c canyon. It is based on the Harlow & Hotchkiss model, and requires
c measured wind speed above the canyon, wind direction and canyon
c geometry.

```

REAL WIND10,Uroof,Ustar,Uh,Vh,
1 W_urb,H1_urb,H2_urb,Uxz,Vz,Wxz,Ures,H,
2 Hc_gmet,Hc_wmet,Hc_gurb,Hc_wurb,Rtop_met,Rtop_urb,
3 KARMAN,Zmix,ORIdrad,ORIddeg,WINDrad,k,beta,gamma,x,y,z

```

```

INTEGER WINDdeg

```

c WIND10 is measured wind speed at ten-metre height (m s-1)
c Uroof is wind speed at roof height (m s-1)
c WINDdeg is wind direction (degrees)
c WINDrad is wind direction (radians)
c Uh is cross-canyon wind speed at roof level (m s-1)
c Vh is down-canyon wind speed at roof level (m s-1)
c H is average height of canyon walls (m)
c W is canyon width (m)
c Uxz is the horizontal component of the in-canyon vortex (m s-1)
c Vz is the along canyon flow at height z in the canyon (m s-1)
c Wxz is the vertical component of the in-canyon vortex (m s-1)
c Ures_d is the resultant wind speed (m s-1)
c Ustar_d is the friction velocity (m s-1)
c KARMAN is the von Karman constant (0.4)
c Zd is the zero-plane displacement (m)
c Z0 is the roughness length (m)
c Zmix is height of bottom of mixed layer (m)

- c ORIrad is direction of canyon axis (radians)
- c z is vertical coordinate of canyon cross-section (m)
- c x is horizontal coordinate of canyon cross-section (m)

- c Universal constants:

$$KARMAN = 0.4$$

$$PI = 3.1415926$$

- c radiation heat transfer coefficient (for sol-air calculations only)

$$U_{roof} = 0.$$

$$WIND_{rad} = \text{float}(WIND_{deg}) * 0.017453$$

- c calculate wind profile from standard wind data at met site:

$$Zd_{met} = 0.001$$

$$Z0_{met} = 0.01$$

$$Zr_{met} = 10.0$$

$$H = 0.5 * (H1_{urb} + H2_{urb})$$

$$Z_{mix} = 2 * H$$

$$U_{star} = WIND10 * KARMAN / (\log((Zr_{met} - Zd_{met}) / Z0_{met}))$$

$$U_{mix} = U_{star} / KARMAN * \log((Z_{mix} - Zd_{met}) / Z0_{met})$$

- c Now calculate surface coefficient for met site:

$$U_{surf_met} = U_{star} / KARMAN * \log((0.2 - Zd_{met}) / Z0_{met})$$

$$Hc_gmet = 6.42 + 3.96 * U_{surf_met}$$

$$Hc_wmet = Hc_gmet$$

- c Calculate Hc for urban canyon:

- c When calculating Hc for the urban canyon surfaces, different

- c values used for ground and walls.

$$OR_{Irad} = OR_{Ideg} * 0.017453$$

- c First calculate wind at roof height from vertical profile.

- c Use approx. ratios for roughness length and displacement height:

$$Zd_{urb} = 0.7 * H$$

$$Z0_{urb} = 0.1 * H$$

$$W = W_{urb}$$

$$U_{roof} = U_{star} / KARMAN * \log((H - Zd_{urb}) / Z0_{urb})$$

$$U_h = U_{roof} * \text{ABS}(\text{SIN}(OR_{Irad} - WIND_{rad}))$$

$$V_h = U_{roof} * \text{ABS}(\text{COS}(OR_{Irad} - WIND_{rad}))$$

- c The following calculations assume a rotor vortex occurs.

- c Wind speed is computed using Hotchkiss and Harlow model:

- c For wind at middle of canyon floor, set:

$$z = 0.2$$

$$x = W/2$$

$$k = \pi/W$$

$$y = z-H$$

$$\beta = \exp(-2*k*H)$$

$$\gamma = \exp(k*y)$$

$$U_{xz} = (U_h/(1-\beta))*(\gamma*(1+k*y)-\beta*(1-k*y)/\gamma)*\sin(k*x)$$

$$V_z = \text{abs}(V_h*(\log(z)/\log(H)))$$

$$W_{xz} = (-U_h*k*y/(1-\beta))*(\gamma-(\beta/\gamma))*\cos(k*x)$$

$$U_{res} = \sqrt{U_{xz}^2 + V_z^2 + W_{xz}^2}$$

$$U_{surf_urb} = U_{res}$$

$$H_c_gurb = 6.42 + 3.96 * U_{res}$$

c For wind at middle of canyon walls, set:

$$z = H/2$$

$$x = 0.2$$

$$k = \pi/W$$

$$y = z-H$$

$$\beta = \exp(-2*k*H)$$

$$\gamma = \exp(k*y)$$

$$U_{xz} = (U_h/(1-\beta))*(\gamma*(1+k*y)-\beta*(1-k*y)/\gamma)*\sin(k*x)$$

$$V_z = \text{abs}(V_h*(\log(z)/\log(H)))$$

$$W_{xz} = (-U_h*k*y/(1-\beta))*(\gamma-(\beta/\gamma))*\cos(k*x)$$

$$U_{res} = \sqrt{U_{xz}^2 + V_z^2 + W_{xz}^2}$$

c Hagishima and Tanimoto correlation for vertical walls:

$$H_c_wurb = 4.47 + 10.2 * u_{res}$$

c -----

c The following sections attempts to model turbulent transfer or
c resistance at canyon top. NOT CAT used in model yet.

c Neutral drag coefficient (Garratt p.54, eq. 3.43):

$$c \quad C_{dn} = \text{KARMAN}^2 / (\log(Z_{mix}/Z_{0_met}))^2$$

c From Garratt, p. 57:

$$c \quad Z_{t_met} = z_{0_met} / 7.4$$

$$c \quad Z_{q_met} = Z_{t_met}$$

$$c \quad C_{hn} = \text{KARMAN}^2 / (\log(Z_{mix}/Z_{t_met}))^2$$

$$c \quad C_{qn} = \text{KARMAN}^2 / (\log(Z_{mix}/Z_{q_met}))^2$$

c calculate transfer resistance to mixed layer above canyon and
c reference site (see Barlow et al,2004 and Garratt, 1992)

c for reference site:

```
IF(Ustar.GT.0.0) THEN
  Rtop_met=(Umix-Usurf_met)/Ustar**2.0
  Rtop_urb=(Umix-Usurf_urb)/Ustar**2.0
ELSE
  Rtop_met=0.002
  Rtop_urb=0.002
END IF

RETURN
END
```

c *****

```
SUBROUTINE PSA (H1,H2,W,H1off,H2off,W1off,W2off,
I ALT,AZI,PI,Iglob,NORw1,PSAg,PSAw1,PSAw2)
```

c This subroutine calculates the partial shaded area of
c canyon surfaces. Canyon geometry allows input of different
c heights for the two canyon walls and for two adjacent buildings,
c each at a different (horizontal) offset from the canyon.

```
INTEGER Iglob
REAL ALT,AZI,PI,
I PSAg,PSAw1,PSAw2,H1,H2,W,NORw1,THETA

LOGICAL SHADEw1,SHADEw2,SHADEadj1,SHADEadj2
```

c ALT is solar altitude (radians)
c AZI is solar azimuth (radians)
c Iglob is global solar radiation on horizontal surface (W m-2)
c PSAg is partial shaded area of the ground
c PSAw1 is partial shaded area of wall 1
c PSAw2 is partial shaded area of wall 2
c W is canyon width (m)
c H1 is height of wall 1 (m)
c H2 is height of wall 2 (m)
c H1off is height of building adjacent to wall 1 (m)
c H2off is height of building adjacent to wall 2 (m)
c W1off is offset of building adjacent to wall 1 (m)
c W2off is offset of building adjacent to wall 2 (m)
c NORw1 is normal to wall 1, the north-facing wall (radians)
c NORw2 is normal to wall 2, the south-facing wall (radians)
c ROOF1_shade is part of roof 1 shaded by adjacent building
c ROOF2_shade is part of roof 2 shaded by adjacent building

```
THETA=ABS(COS(NORw1-AZI))
```

c THETA is the absolute value of the cosine of the angle
c between solar azimuth and the normal to the canyon wall.
c If AZI is represented as radians east or west of north,
c then $ABS(COS(NORw1-AZI))=ABS(COS(NORw2-AZI))=THETA$
c for all orientations.

c First test to see if sun is above the horizon,
c or if there is global radiation.

c Then test to see which of the canyon walls
c is shaded from direct solar radiation because of azimuth.

c
c initialise variables
SHADEadj1 = .FALSE.
SHADEadj2 = .FALSE.

c
IF((ALT.LE.0).or.(Iglob.EQ.0)) THEN
PSAg=1
PSAw1=1
PSAw2=1
GOTO 98
ENDIF

IF (ABS(NORw1-AZI).LT.PI/2) THEN
SHADEw1=.FALSE.
SHADEw2=.TRUE.
ELSE
SHADEw1=.TRUE.
SHADEw2=.FALSE.
ENDIF

c Now test for shade by adjacent buildings

ROOF1_shade=(H1off-H1)*THETA/TAN(ALT)
IF (ROOF1_shade.GT.W1off) SHADEadj1=.TRUE.

ROOF2_shade=(H2off-H2)*THETA/TAN(ALT)
IF (ROOF2_shade.GT.W2off) SHADEadj2=.TRUE.

c PSA of canyon floor:

IF (SHADEw1) THEN
IF (SHADEadj1) THEN
PSAg=((H1off*THETA/TAN(ALT))-W1off)/W
ELSE
PSAg=(H1/W)*(THETA/TAN(ALT))
ENDIF
ELSE
IF (SHADEadj2) THEN
PSAg=((H2off*THETA/TAN(ALT))-W2off)/W
ELSE
PSAg=(H2/W)*(THETA/TAN(ALT))
ENDIF
ENDIF
PSAg=ABS(PSAg)

c PSA of wall 1:

c (First check if it is shaded by azimuth)

IF (SHADEw1) THEN
PSAw1=1
ELSE
IF (.NOT.(SHADEw1).AND.(PSAg.GT.1)) THEN
IF (SHADEadj1) THEN
PSAw1=(H2off-(TAN(ALT)/THETA)*(W+W2off))/H1
ELSE

```

    PSAw1=(H2-W*(TAN(ALT)/THETA))/H1
  ENDIF
ELSE
  PSAw1=0
ENDIF
ENDIF
PSAw1=ABS(PSAw1)

```

- c PSA of wall 2:
- c (First check if it is shaded by azimuth)

```

IF (SHADEw2) THEN
  PSAw2=1
ELSE
  IF (.NOT.(SHADEw2).AND.(PSAg.GT.1)) THEN
    IF (SHADEadj2) THEN
      PSAw2=(H1off-(TAN(ALT)/THETA)*(W+W1off))/H2
    ELSE
      PSAw2=(H1-W*(TAN(ALT)/THETA))/H2
    ENDIF
  ELSE
    PSAw2=0
  ENDIF
ENDIF
PSAw2=ABS(PSAw2)

```

```

IF (PSAg.GT.1) PSAg=1
IF (PSAw1.GT.1) PSAw1=1
IF (PSAw2.GT.1) PSAw2=1

```

```

98 RETURN
END

```

c -----

```

SUBROUTINE SENSIBLE (SITE,Ta,Qstar,Qstar_prev,dQstar,dQs,Qh,Qe,
  I alpha,A1,A2,A3,RAIN,RAIN_prev)

```

```

REAL Qstar,dQstar,Qstar_prev,dQs,Qh,Qe,
  I alpha,beta,gamma,s,es,A1,A2,A3,alphad,RAIN

```

```

INTEGER SITE

```

```

LOGICAL RAIN_prev

```

- c This subroutine computes the storage flux (dQs) at a surface from
- c the net radiant flux Qstar using the OHM model by Grimmond and Oke.
- c The storage flux is then used to calculate the sensible heat flux
- c from the surface, using the expression from Grimmond and Oke (2002).

- c dQs is storage flux (W m-2)
- c es is saturation vapour pressure (kPa)
- c Qh is sensible heat flux (W m-2)
- c Qstar is net radiant flux (W m-2)
- c dQstar is the change in net radiant flux over the previous hour
- c Qstar_prev is net radiant flux in the previous time step (W m-2)

- c s is the slope of the saturation vapour pressure vs. temperature
- c Ta is air dry bulb temperature (deg C)
- c alpha, beta and gamma are coefficients in the expression for Qh
- c A1,A2 and A3 are coefficients in the OHM model for storage flux
- c SITE is flag for reference or urban
- c RAIN is rainfall at weather station in current hour
- c RAIN_prev is TRUE if it rained (>0.5mm) in the previous hour
- c alphad is the dynamic rain-corrected value of alpha

```
IF(SITE.EQ.4) THEN
  beta=10.0
ELSE IF (SITE.EQ.7) THEN
  beta=3
END IF
```

- c beta=20

- c gamma the psychometric constant (kPa K-1)

```
gamma=0.065
```

- c First calculate storage flux (dQs):

```
dQstar = Qstar-Qstar_prev
```

```
dQs=a1*Qstar+a2*dQstar+a3
```

- c Now calculate atmospheric properties required to parcel
- c turbulent heat flux into sensible and latent components.
- c Saturation vapour pressure (kPa) is calculated using the Tetens formula:
- c (Tetens, 1930; as expressed by Murray, 1967)

```
es=0.61078*EXP((17.269*Ta)/(Ta+237.29))
```

- c 's', the slope of the saturation vapour pressure versus temperature
- c curve:

```
s = es*4099./(Ta+237.3)**2.
```

- c Alternative formulation using Monteith equation 2.24.
- c Units of gamma and s are in Pa K-1, not KPa K-1.

- c gamma=65
- c TaK=Ta+273.15
- c s=es*2439500*18.015/(8.31*TaK**2)

- c Sensible heat flux is parameterised from net radiation and storage
- c using revised format by Grimmond and Oke (2002).
- c The value of alpha, the coefficient of moisture availability,
- c is increased after rain, to model increased latent heat flux.

```
IF(RAIN.GT.0.5.OR.RAIN_prev) THEN
  IF(SITE.EQ.4) THEN
    alphad=alpha+0.01
  ELSE IF (SITE.EQ.7) THEN
```

```

    alphad=alpha+0.10
  END IF
ELSE
  alphad=alpha
END IF

```

$$Q_h = (((1 - \text{alphad}) + (\gamma/s)) / (1 + (\gamma/s))) * (Q_{\text{star}} - dQ_s) - \beta$$

$$Q_e = (\text{alphad} / (1 + (\gamma/s))) * (Q_{\text{star}} - dQ_s) + \beta$$

c Reset value of alphad before next hourly period:

```

  alphad=alpha

```

```

  RETURN
  END

```

c -----

```

SUBROUTINE deltaT
  1 (Hsurf,Qh,dTa,MIX,SURFonW,Vol,MIXING,dTsol,Qe,dMC)

```

```

  REAL Hsurf,Qh,MIX(4),dTa,MIXING,SURFonW,dTsol

```

c Following variables required for moisture calculations.

c These are currently disabled.

c REAL dTvap

c This subroutine calculates the change in localized air temperature

c resulting from the sensible heat flux at the surface, taking into

c account empirical mixing factors to describe the effects of

c buoyancy and mechanical turbulence near the surface.

```

  mix(1)=0.61
  mix(2)=0.76
  mix(3)=0.81
  mix(4)=0.92

```

```

  IF(dTsol.lt.-2.0) THEN
    mixing=mix(1)
    else if ((dTsol.lt.0.0).AND.(dTsol.ge.-2.0)) then
      mixing=mix(2)
    else if ((dTsol.lt.5.0).AND.(dTsol.ge.0.0)) then
      mixing=mix(3)
    else if (dTsol.gt.5) then
      mixing=mix(4)
  END IF

```

c $dT_a = Q_h * ((1 - \text{mixing}) / ((\text{SURFonW} * H_{\text{surf}}) + H_{\text{top}}))$

```

  Rsurf=1/(SurfonW*Hsurf)
  Rtop=0.000
  Rtot=Rsurf+Rtop

```

$$dT_a = Q_h * (1 - \text{mixing}) * R_{\text{tot}}$$

c
c The following section is NOT finished: speculates on methods
c to model changes in moisture content.
c

c heat of vapourisation of water (KJ/kg)
dTvap=2450
c density of air kg/m3
dens = 1.2

c Qsurf is the transfer coefficient for moisture,
c analogous to Hsurf. Ratio depends on z0. Value of 1.3 is
c for z0=0.01m.

$$Q_{surf} = H_{surf} * 1.3$$

$$dMc = (3600 * (1 - mixing) * Q_e / dTvap) / (Q_{surf} * Vol * dens * 1000.)$$

c dMc = ((1 - mixing) * Q_e) / (Q_surf * VOL)

c End of speculative section.

RETURN
END

c -----

SUBROUTINE SITEDATA

1 (SITE,albed,W,H1,H2,W1off,H1off,W2off,H2off,
2 ORIddeg,A1,A2,A3)

REAL albed(2),H1,H2,W,H1off,H2off,W1off,W2off
REAL A1(3),A2(3),A3(3)

INTEGER SITE

c This subroutine reads data required for urban heat island effect
c calculations from input files met_site.txt or urb_site.txt

60 FORMAT(60x,f7.2)

c read past header and star line
READ(SITE,*)
READ(SITE,*)
READ(SITE,*)

c Read urban cluster properties:

READ(SITE,60) albed(1)
READ(SITE,60) albed(2)
READ(SITE,60) W
READ(SITE,60) H1
READ(SITE,60) H2
READ(SITE,60) W1off
READ(SITE,60) H1off
READ(SITE,60) W2off

```

READ(SITE,60) H2off
READ(SITE,60) ORIdeg
c READ(SITE,60) alpha
READ(SITE,60) A1(1)
READ(SITE,60) A2(1)
READ(SITE,60) A3(1)
READ(SITE,60) A1(2)
READ(SITE,60) A2(2)
READ(SITE,60) A3(2)
READ(SITE,60) A1(3)
READ(SITE,60) A2(3)
READ(SITE,60) A3(3)

c display data for checking

write(6,61)albed(1)
61 format(' Mean surface albedo ground ',f5.2)

write(6,62)albed(2)
62 format(' Mean surface albedo walls ',f5.2)

write(6,63)W
63 format(' Canyon width, in metres (W) ',f5.2)

write(6,64)H1
64 format(' Height of wall 1, in metres (H1) ',f5.2)

write(6,65)H2
65 format(' Height of wall 2, in metres (H2) ',f5.2)

write(6,66)W1off
66 format(' Offset of building adjacent to wall 1 ',f5.2)

write(6,67)H1off
67 format(' Height of building adjacent to wall 1 ',f5.2)

write(6,68)W2off
68 format(' Offset of building adjacent to wall 2 ',f5.2)

write(6,69)H2off
69 format(' Height of building adjacent to wall 2 ',f5.2)

c write(6,70)alpha
c 70 format(' Empirical coefficient for soil moisture ',f5.2)

write(6,71)A1(1)
71 format(' Heat storage coefficient A1 ground ',f5.2)

write(6,72)A2(1)
72 format(' Heat storage coefficient A2 ground ',f5.2)

write(6,73)A3(1)
73 format(' Heat storage coefficient A3 ground ',f5.1)

write(6,74)A1(2)
74 format(' Heat storage coefficient A1 wall 1 ',f5.2)

write(6,75)A2(2)
75 format(' Heat storage coefficient A2 wall 1 ',f5.2)

```

```

write(6,76)A3(2)
76 format(' Heat storage coefficient A3 wall 1      ',f5.1)

write(6,77)A1(3)
77 format(' Heat storage coefficient A1 wall 2      ',f5.2)

write(6,78)A2(3)
78 format(' Heat storage coefficient A2 wall 2      ',f5.2)

write(6,79)A3(3)
79 format(' Heat storage coefficient A3 wall 2      ',f5.1)

```

pause ' Check data, then press ENTER to continue.'

```

RETURN
END

```

c -----

```

subroutine moisture (pt,t,rh,w)

```

```

REAL pt,t,w,ps,p,psw
INTEGER rh

```

c This subroutine calculates the moisture content of air from
c dry bulb temperature and relative humidity.

c (Total atmospheric pressure also required - if not available,
c use Pt=1013.25 mb.)

c p is actual pressure of water vapour (kPa)
c ps is saturated pressure of water vapour (kPa)
c psw is saturated pressure of water vapour at the TWB (kPa)
c pt is total atmospheric pressure (kPa)
c rh is relative humidity (%)
c t is dry bulb temperature (deg C)
c w is moisture content of air (g of water per kg of dry air)

c TWB - thermodynamic wet bulb temperature

```

ps = psw(t)
c PRINT*, ' ps (mhar) = ',ps
P = 0.01*rh*ps

FS=-7.3E-06*t+1.00444
IF(t.GE.11.0.AND.t.LT.26.0) FS=1.32E-05*t+1.004205
IF(t.GE.26.0) FS=4.05E-05*t+1.003497

w = 1000*0.622*FS*p/(pt-FS*p)

return
end

```

c -----

```

SUBROUTINE MOMENT(DATA,N,AVE,ADEV,SDEV,VAR,SKEW,CURT)

```

```

DIMENSION DATA(N)
IF(N.LE.1)PAUSE 'N must be at least 2'
S=0.
DO 11 J=1,N
  S=S+DATA(J)
11 CONTINUE
AVE=S/N
ADEV=0.
VAR=0.
SKEW=0.
CURT=0.
DO 12 J=1,N
  S=DATA(J)-AVE
  ADEV=ADEV+ABS(S)
  P=S*S
  VAR=VAR+P
  P=P*S
  SKEW=SKEW+P
  P=P*S
  CURT=CURT+P
12 CONTINUE
ADEV=ADEV/N
VAR=VAR/(N-1)
SDEV=SQRT(VAR)
IF(VAR.GT.1E-08)THEN
  SKEW=SKEW/(N*SDEV**3)
  CURT=CURT/(N*VAR**2)-3.
ELSE
  PAUSE 'no skew or kurtosis when zero variance'
ENDIF
RETURN
END

c
c *****
c
SUBROUTINE FIT(X,Y,NDATA,SIG,MWT,A,B,SIGA,SIGB,CHI2,Q)
DIMENSION X(NDATA),Y(NDATA),SIG(NDATA)

c
c PRINT*, ndata
c
SX=0.
SY=0.
ST2=0.
B=0.
IF(MWT.NE.0) THEN
  SS=0.
  DO 11 I=1,NDATA
    WT=1./(SIG(I)**2)
    SS=SS+WT
    SX=SX+X(I)*WT
    SY=SY+Y(I)*WT
11 CONTINUE
ELSE
  DO 12 I=1,NDATA
    SX=SX+X(I)
    SY=SY+Y(I)
12 CONTINUE
  SS=FLOAT(NDATA)
ENDIF
SXOSS=SX/SS

```



```

IF(MWT.NE.0) THEN
  DO 13 I=1,NDATA
    T=(X(I)-SXOSS)/SIG(I)
    ST2=ST2+T*T
    B=B+T*Y(I)/SIG(I)
13  CONTINUE
  ELSE
    DO 14 I=1,NDATA
      T=X(I)-SXOSS
      ST2=ST2+T*T
      B=B+T*Y(I)
14  CONTINUE
  ENDF
  B=B/ST2
  A=(SY-SX*B)/SS
  SIGA=SQRT((1.+SX*SX/(SS*ST2))/SS)
  SIGB=SQRT(1./ST2)
  CHI2=0.
  IF(MWT.EQ.0) THEN
    DO 15 I=1,NDATA
      CHI2=CHI2+(Y(I)-A-B*X(I))**2
15  CONTINUE
    Q=1.
    SIGDAT=SQRT(CHI2/(NDATA-2))
    SIGA=SIGA*SIGDAT
    SIGB=SIGB*SIGDAT
  ELSE
    DO 16 I=1,NDATA
      CHI2=CHI2+((Y(I)-A-B*X(I))/SIG(I))**2
16  CONTINUE
    Q=GAMMQ(0.5*(NDATA-2),0.5*CHI2)
  ENDF
  RETURN
END

c
FUNCTION GAMMQ(A,X)
IF(X.LT.0..OR.A.LE.0.)PAUSE
IF(X.LT.A+1.)THEN
  CALL GSER(GAMSER,A,X,GLN)
  GAMMQ=1.-GAMSER
ELSE
  CALL GCF(GAMMCF,A,X,GLN)
  GAMMQ=GAMMCF
ENDF
RETURN
END

c
SUBROUTINE GSER(GAMSER,A,X,GLN)
PARAMETER (ITMAX=100,EPS=3.E-7)
GLN=GAMMLN(A)
IF(X.LE.0.)THEN
  IF(X.LT.0.)PAUSE
  GAMSER=0.
  RETURN
ENDF
AP=A
SUM=1./A
DEL=SUM
DO 11 N=1,ITMAX
  AP=AP+1.

```

```

      DEL=DEL*X/AP
      SUM=SUM+DEL
      IF(ABS(DEL).LT.ABS(SUM)*EPS)GO TO 1
11  CONTINUE
      PAUSE 'A too large, ITMAX too small'
1   GAMSER=SUM*EXP(-X+A*LOG(X)-GLN)
      RETURN
      END
c
      SUBROUTINE GCF(GAMMCF,A,X,GLN)
      PARAMETER (ITMAX=100,EPS=3.E-7)
      GLN=GAMMLN(A)
      GOLD=0.
      A0=1.
      A1=X
      B0=0.
      B1=1.
      FAC=1.
      DO 11 N=1,ITMAX
      AN=FLOAT(N)
      ANA=AN-A
      A0=(A1+A0*ANA)*FAC
      B0=(B1+B0*ANA)*FAC
      ANF=AN*FAC
      A1=X*A0+ANF*A1
      B1=X*B0+ANF*B1
      IF(INT(A1).NE.0)THEN
      FAC=1./A1
      G=B1*FAC
      IF(ABS((G-GOLD)/G).LT.EPS)GO TO 1
      GOLD=G
      ENDIF
11  CONTINUE
      PAUSE 'A too large, ITMAX too small'
1   GAMMCF=EXP(-X+A*ALOG(X)-GLN)*G
      RETURN
      END
c
      FUNCTION GAMMLN(XX)
      REAL*8 COF(6),STP,HALF,ONE,FPF,X,TMP,SER
      DATA COF,STP/76.18009173D0,-86.50532033D0,24.01409822D0,
1   -1.231739516D0,.120858003D-2,-.536382D-5,2.50662827465D0/
      DATA HALF,ONE,FPF/0.5D0,1.0D0,5.5D0/
      X=XX-ONE
      TMP=X+FPF
      TMP=(X+HALF)*LOG(TMP)-TMP
      SER=ONE
      DO 11 J=1,6
      X=X+ONE
      SER=SER+COF(J)/X
11  CONTINUE
      GAMMLN=TMP+LOG(STP*SER)
      RETURN
      END
c
c *****
      subroutine WILLMOTT(P,O,Ndata,A,B,RMSE,RMSEs,RMSEu,d,
1 MSE,MSEs,MSEu)
c
      REAL P(9000),O(9000),PHat(9000),MSE,Pd(9000),Od(9000),MSEs,MSEu

```

```

c
c initialize SUMs
  SUM1=0.
  SUM2=0.
  SUM3=0.
  SUMm=0.
  PE=0.
c calculate Mean of O
  do 5 i=1,Ndata
    SUMm = SUMm + O(i)
  5  continue
  Omean = SUMm/Ndata
c PRINT*, Omean
c
c calculate PHat
c
  do 10 i=1,Ndata
    PHat(i) = A + B*O(i)
  10 continue
c
  do 20 i=1,Ndata
    SUM1 = SUM1+ (PHat(i) - O(i))**2
  20 continue
  MSEs = SUM1/Ndata
  RMSEs = SQRT(SUM1/Ndata)
c
  do 30 i=1,Ndata
    SUM2 = SUM2+ (P(i) - PHat(i))**2
  30 continue
  MSEu = SUM2/Ndata
  RMSEu = SQRT(SUM2/Ndata)
c
  do 40 i=1,Ndata
    SUM3 = SUM3+ (P(i) - O(i))**2
  40 continue
c PRINT*,sum3
  MSE = SUM3/Ndata
  RMSE = SQRT(MSE)
c
  do 50 i=1,Ndata
    Pd(i) = P(i) - Omean
  50 continue
c
  do 60 i=1,Ndata
    Od(i) = O(i) -Omean
  60 continue
c
  do 70 i=1,Ndata
    PE = PE + (ABS(Pd(i)) +ABS(Od(i)))**2
  70 continue
c
  d = 1. - Ndata*MSE/PE
c
  RETURN
  END

c *****

```

```

subroutine CONFIRM(P,O,V,Ndata,U,D)

REAL P(9000),O(9000),V(9000)

c initialise sum variables
SUMp =0.
SUMo =0.
SUMv =0.
SUM1 =0.
SUM2 =0.

do 10 i=1,Ndata
SUMp = SUMp + P(i)**2.
10 continue
SUMp =SUMp/Ndata

do 20 i=1,Ndata
SUMo = SUMo + O(i)**2.
20 continue
SUMo = SUMo/Ndata

do 30 i=1,Ndata
SUMv = SUMv + V(i)**2.
30 continue
SUMv = SUMv/Ndata

do 40 i=1,Ndata
SUM1 = SUM1+ (P(i) - O(i))**2.
40 continue

c inequality coefficiency (U(p,o))
aNUM1 = SQRT(SUM1/Ndata)
U = aNUM1/(SQRT(SUMp)+SQRT(SUMo))

do 50 i=1,Ndata
SUM2 = SUM2 + (O(i) - V(i))**2.
50 continue

c inequality coefficient (U(o,v))
aNUM2 =SQRT(SUM2/Ndata)
Uov = aNUM2/(SQRT(SUMo)+SQRT(SUMv))

c Confirmation co-efficient (U(o,v)-U(p,o))/U(o,v)
D = (Uov-U)/Uov

RETURN
END

c -----

subroutine TandW(t,w,rh)

real pt,t,w,ps,p
integer rh

c Calculate RH (and other parameters) from dry bulb temperature t (C)
c and moisture content of air w (g of water/kg of dry air)

```

```
c *****  
c Note: w given in grams!  
c *****
```

```
c Total atmospheric pressure:  
pt=1013.25
```

```
c h = 1.0048*t+(1.8003*t+2502.68)*w;  
c v = 6.89476*0.062428*(491.7+1.8*t)*(0.622+w)/(1.679*pt);  
c tw = WB(pt,t,w);  
c psw = p1(tw);  
c ws = 0.622*psw/(pt-psw);  
c td = DP(p);
```

```
p = w*1E-03*pt/(0.622+w*1E-03)  
ps = psw(t)  
rh = INT(100.0*p/ps)
```

```
end
```

```
c  
FUNCTION psw(t)
```

```
c calculate saturated pressure of water vapour (psw) at temperature t  
c psw mbar (hPa)
```

```
c  
x = 673.4 - 1.8*DBLE(t)  
psw = (6.89476*3206.18/exp(2.302585*x*(3.2437814+3.26014E-3*x  
+2.00658E-9*x**3.)/((1165.09-x)*(1.0+1.21547e-3*x))))*10.
```

```
return  
end
```

NOTE:

Canyon Air Temperature v.1.0
CD-ROM is included with the print
copy of the thesis held in the
University of Adelaide Library